

Catalytic Locomotion of Core–Shell Nanowire Motors

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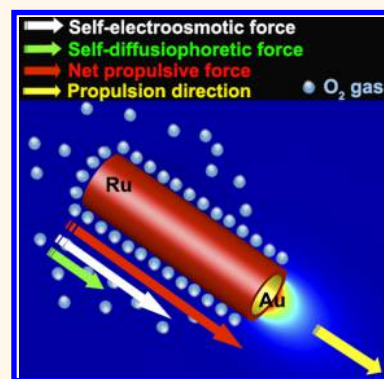
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Supporting Information

ABSTRACT: We report Au/Ru core–shell nanowire motors. These nanowires are fabricated using our previously developed electrodeposition-based technique, and their catalytic locomotion in the presence of H_2O_2 is investigated. Unlike conventional bimetallic nanowires that are self-electroosmotically propelled, our open-ended Au/Ru core–shell nanowires show both a noticeable decrease in rotational diffusivity and increase in motor speed with increasing nanowire length. Numerical modeling based on self-electroosmosis attributes decreases in rotational diffusivity to the formation of toroidal vortices at the nanowire tail, but fails to explain the speed increase with length. To reconcile this inconsistency, we propose a combined mechanism of self-diffusiophoresis and electroosmosis based on the oxygen gradient produced by catalytic shells. This mechanism successfully explains not only the speed increase of Au/Ru core–shell nanomotors with increasing length, but also the large variation in speed among Au/Ru, Au/Rh, and Rh/Au core–shell nanomotors. The possible contribution of diffusiophoresis to an otherwise well-established electroosmotic mechanism sheds light on future designs of nanomotors, at the same time highlighting the complex nature of nanoscale propulsion.

KEYWORDS: electrodeposition, core–shell nanowires, catalytic nanomotors, self-electroosmosis, self-diffusiophoresis, net propulsive force



Fifteen years ago, Whitesides *et al.* pioneered self-propelled catalytic millimeter-scale ships,¹ triggering the development of synthetic micro- and nanomotors. These devices move autonomously in the presence of a fuel solution by converting chemical to mechanical energy.² Most reported catalytic micro- and nanomotors are driven by the decomposition of hydrogen peroxide, although examples using glucose and urea as fuel have been reported recently.^{3–6} Several applications for these miniaturized motors have been demonstrated, such as electronic circuit healing,⁷ biosensing,^{4,8} nanolithography,⁹ microfluidic pumping,¹⁰ nanocargo transport,¹¹ and environmental remediation (for details, see recent review articles).^{12–17} Most of these applications require precise control over the speed and directionality of the motors,¹⁸ which are highly dependent on motor design parameters, such as geometry, size and composition. Understanding the mechanisms involved in the propulsion of catalytic micro- and nanomotors as a function of their design is crucial for controlling their motion. Different propulsion mechanisms have been identified, such as bubble propulsion, self-electroosmosis, self-diffusiophoresis, and interfacial tension.¹⁷ In the

first mechanism, bubbles are formed on the catalytic surface and impart momentum to the motor. For example, tubular microjets are driven by oxygen bubble propulsion, caused by the decomposition of H_2O_2 at the inner catalytic surface.^{19,20} While bubble propulsion seems the most intuitive way to explain the motion of these motors, this mechanism cannot be used to rationalize, for instance, the motion of bimetallic structures, such as Pt/Au or Cu/Pt nanowires (NWs) in H_2O_2 and I_2 solutions, respectively.^{21,22} For bimetallic NWs, self-electroosmosis is generally the most accepted mechanism.^{22,23} In this case, a self-induced electric field is generated by redox reactions occurring on the two different metallic segments. The motion of other micro- and nanomotors has been explained in terms of self-diffusiophoresis. Several efforts suggest that micro- and nanoparticles asymmetrically coated with Pt move due to an O_2 concentration gradient caused by the asymmetric

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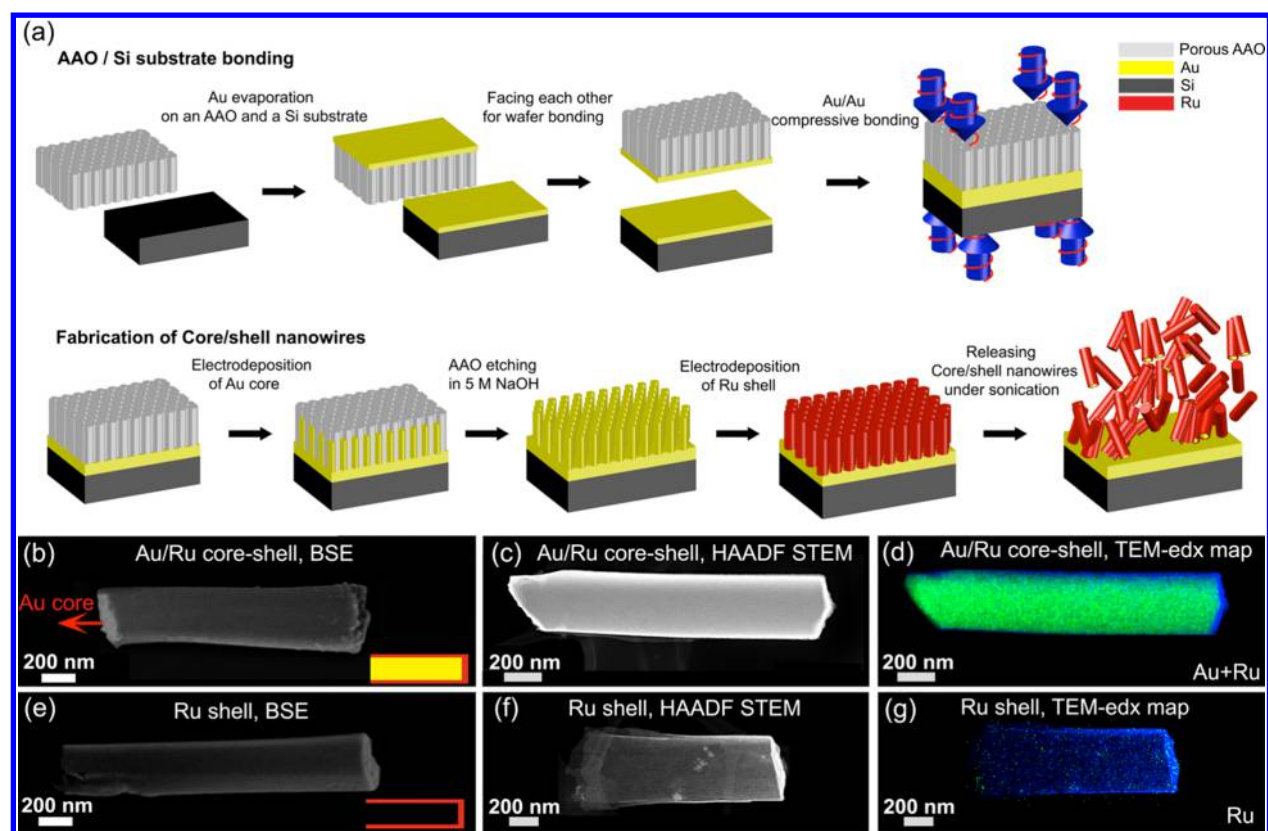


Figure 1. (a) A schematic drawing of the fabrication of core–shell NWs. The fabrication process includes AAO/Si substrate bonding and electrodeposition. BSE images of (b) a Au/Ru core–shell NW and (e) a Ru shell. Insets in (b) and (e) are schematic drawings of Au/Ru core–shell NW and Ru shell, respectively. HAADF STEM images of (c) a Au/Ru core–shell NW and (f) a Ru shell. TEM-EDX maps of (d) a Au/Ru core–shell NW and (g) a Ru shell, respectively.

decomposition of H_2O_2 along the body of the motor.^{24–28} Recent investigations evaluating more complex motor architectures indicate a concomitant occurrence of mechanisms.^{29–31}

Among all micro- and nanomotor structures, NWs are particularly appealing due to their unique physical properties.³² Additionally, NWs can be compartmentalized in several functional modules by means of segmentation^{33,34} or coaxial lithography³⁵ to increase their capabilities. For instance, the trajectory of a catalytic NW motor consisting of Pt/Ni/Au/Ni/Au segments can be controlled by means of magnetic fields.³⁶ However, interfacing certain building blocks can be detrimental for several applications. For example, the combination of two dissimilar metallic segments, such as Au and Ni, can lead to an increase of the corrosion rate of the magnetic part due to galvanic coupling.³⁷ Also, the interaction of certain materials (e.g., Ni) with the surrounding environment (e.g., biological or aquatic media) must be avoided to prevent undesired leakage of toxic ions. Alternatively, a core–shell arrangement can provide an inert housing to shield certain components from the surrounding environment. Core–shell NWs have been manufactured using a wide variety of methods, which usually require two or more steps.^{38–43} However, a purely core–shell structure, by definition, cannot become a motor due to the inherent absence of broken symmetry in composition. By comparison, a conventional NW motor (e.g., Au/Pt bimetallic rods in H_2O_2) has both of their surfaces exposed to the solution and thus propels. A partial core–shell nanomotor that can shelter the active components while generating asymmetric propulsion is, therefore, desired but challenging.

In this work, we synthesized open-ended core–shell nanomotors with one side of the core exposed to solutions, by capitalizing on a recently developed method that allows for the batch fabrication of freestanding NWs based on template-assisted electrodeposition and wafer bonding. As the NWs were self-supported on the wafer after template removal, a second electrodeposition step produced a core–shell architecture. These core–shell NWs were, then, sonicated off from the substrate, exposing the first (therefore, core) material to the solution at the breaking point. This developed method can be adopted to fabricate core–shell NWs with various material combinations. Here, we synthesized different types of bimetallic core–shell NWs, such as Au/Ru, Rh/Au, and Au/Rh (core/shell), and investigated their motion in H_2O_2 solutions. Importantly, abnormal behaviors were found, including a speed increase with the length of Au/Ru core–shell NWs and a large speed difference among Au/Ru, Rh/Au, and Au/Rh. These behaviors are not observed for conventional bimetallic NWs, and, therefore, cannot be accounted for solely by self-electroosmosis. To understand these unusual trends, we propose a combined mechanism of self-diffusiophoresis and electroosmosis based on the oxygen gradient produced by catalytic shells, which successfully explain all experimental observations.

RESULTS/DISCUSSION

Design and Fabrication of the Au/Ru Core–Shell NWs. The fabrication process is illustrated in Figure 1a. First, an anodic aluminum oxide (AAO) membrane was transferred

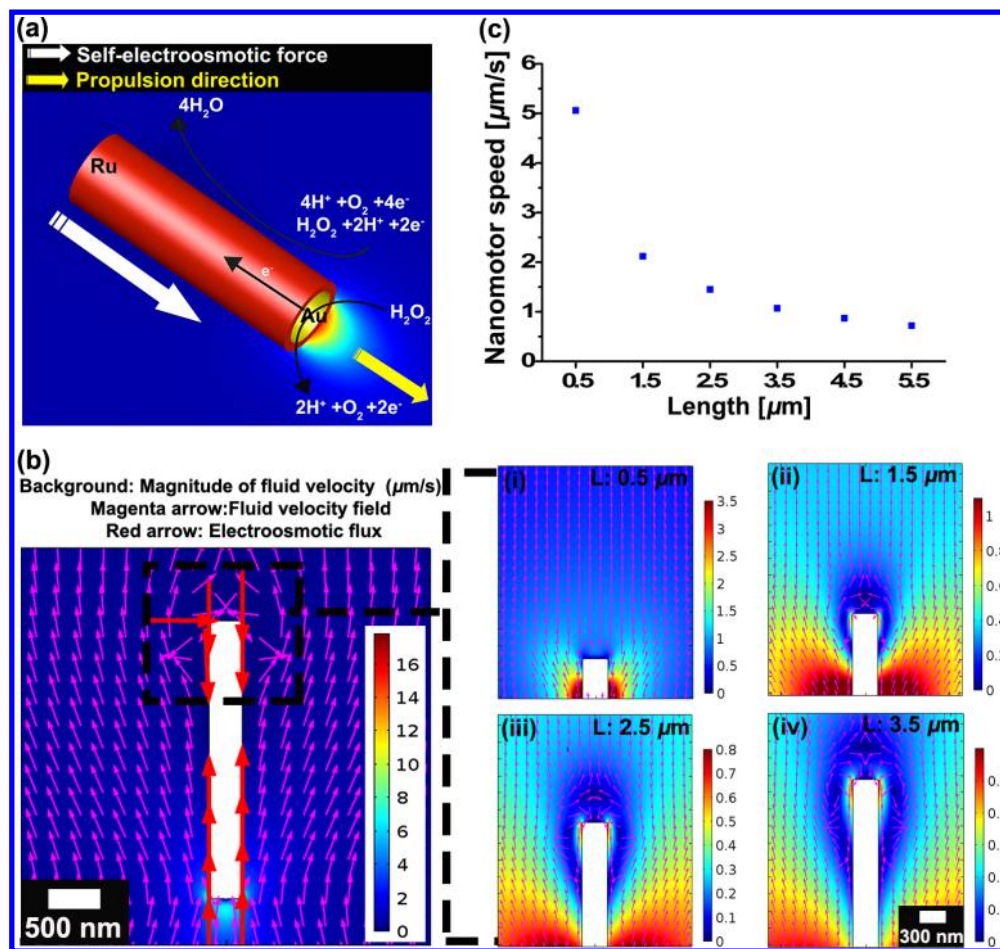


Figure 2. Numerical modeling of Au/Ru core–shell NW in the presence of H_2O_2 . (a) A schematic drawing of the self-electroosmosis model for our Au/Ru core–shell NW. The force arrow is represented from the point of view of the nanomotor rather than the fluid. (b) Magnitude of fluid velocity (background), fluid velocity (magenta arrows), and electroosmotic flux (red arrows) of Au/Ru core–shell NW with a length of $2.5 \mu\text{m}$; the insets are the magnified images of the magnitude of fluid velocity (background) and fluid velocity field (magenta arrows) for the length of (i) $0.5 \mu\text{m}$, (ii) $1.5 \mu\text{m}$, (iii) $2.5 \mu\text{m}$, and (iv) $3.5 \mu\text{m}$; the diameter of NWs are fixed to 300 nm . (c) Speed as a function of length.

onto a Si substrate *via* the Au/Au compressive bonding technique previously developed in our group.⁴⁴ Next, Au was electrodeposited into the pores of the AAO. The AAO was then chemically etched to obtain a freestanding Au NW array on the Si substrate. Ru was then electrochemically deposited on the freestanding Au NW array, resulting in the formation of a core–shell structure. The strong adhesion between the freestanding array and the Si substrate is able to withstand the electroosmotic and fluidic forces exerted on the NWs during Ru electrodeposition. The freestanding NWs must be kept in solution to prevent drying, because the surface tension forces during drying will cause severe NW aggregation⁴⁵ and result in a nonuniform deposition of the Ru shell. After the Ru deposition, the NWs were released by sonication.

The scanning electron microscope (SEM) image in Figure 1b, obtained using a backscattered electron (BSE) detector, shows a typical Au/Ru core–shell NW with an approximate diameter and length of 350 nm and $2.5 \mu\text{m}$, respectively, where the length varies with the deposition time of the Au core. Since the intensity of the BSE signal is proportional to the atomic number, the bright area and the dark area can be assigned to Au and Ru, respectively. The Au core appears only at the base (left end) as a consequence of being released from the Si substrate. No obvious defects are observed in the Au/Ru core–shell NW structure, as is seen in the high-angle annular dark field

(HAADF) scanning transmission electron microscopy (STEM) image (Figure 1c). The corresponding energy dispersive X-ray (EDX) mapping verifies that the core–shell NW is composed of Au and Ru (Figure 1d). For a better understanding of the Ru distribution, we then selectively etched the Au core in Au etchant. Representative SEM and STEM images (Figure 1e,f) show that the remaining structure after etching is a Ru shell. The Ru shell has an approximate diameter of 350 nm , which is similar to that of a Au/Ru core–shell NW. A smooth surface of the nanoshell without holes or cracks on the rod is observed and confirms the uniform distribution and the conformal growth of the Ru shell. Subsequent EDX mapping verifies that the nanoshell solely consists of Ru (Figure 1g). The structures of a conventional bimetallic nanorod, a purely core–shell NW, and our open-ended core–shell NW are given in Figure S1 to highlight the difference in their structures. We note that “core–shell NW” is used to refer to our open-ended core–shell structure from here on for the sake of simplicity.

Numerical Modeling of Electroosmotic Mechanism of Core–Shell NWs. Electroosmosis is the main driving force for locomotion based on surface redox reactions.^{46,47} The redox reaction consists of an oxidation reaction and reduction reaction, as illustrated in Figure 2a. Protons, oxygen molecules, and electrons are generated in the oxidation process at the anode (Au) by decomposing H_2O_2 . The generated protons

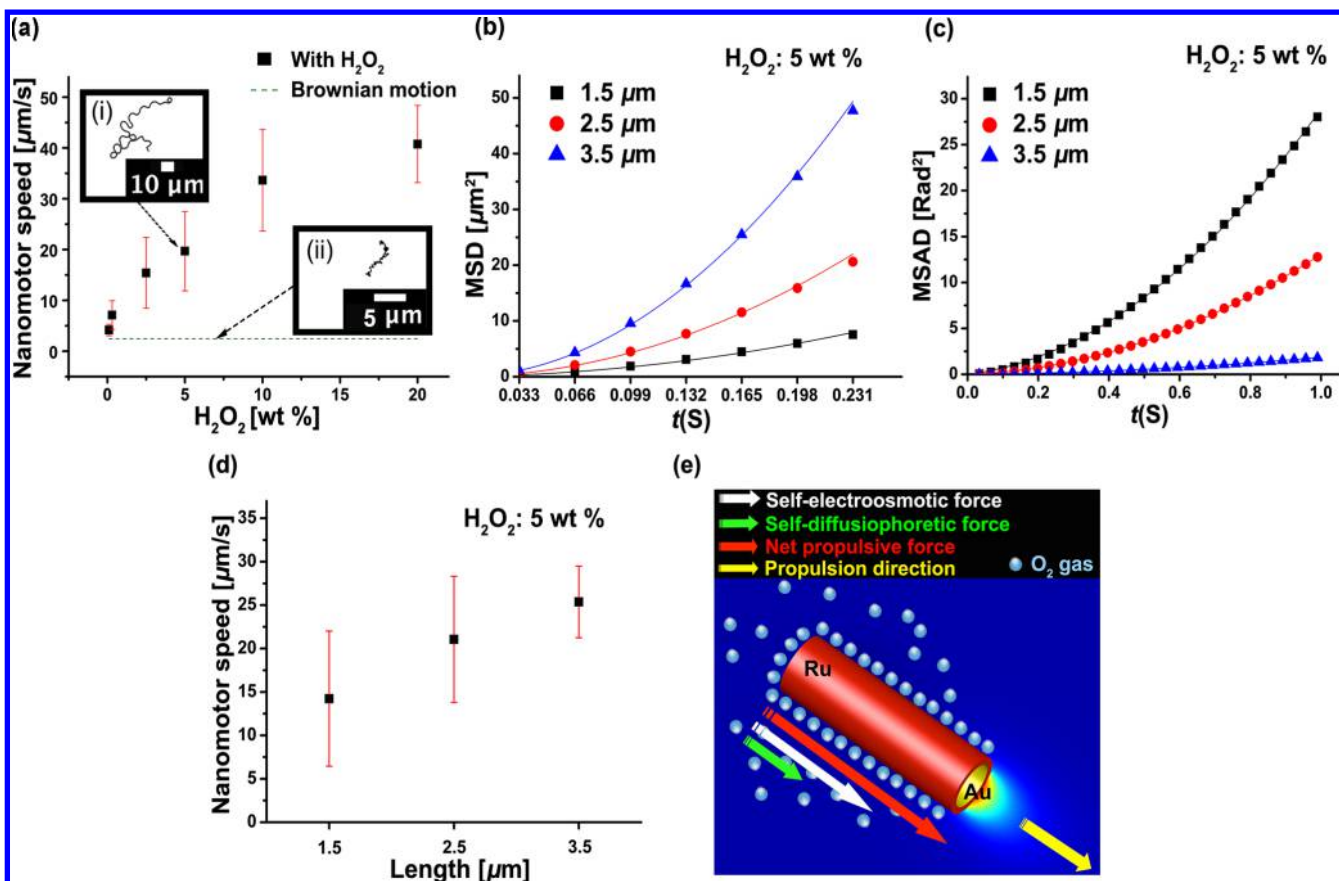


Figure 3. Experimental data of Au/Ru core-shell NW in the presence of H₂O₂. (a) Average speed as a function of the concentration of H₂O₂ for NWs with an approximate length of 2.5 μm . Inset: trajectories of a core-shell NW at (i) 5 wt % H₂O₂ and (ii) 0 wt % H₂O₂. The averaged (b) MSD and (c) MSAD curves of Au/Ru core-shell NWs at different lengths (1.5, 2.5, and 3.5 μm). Scatters represent averaged MSD or MSAD values, and lines represent fits. (d) Speed of Au/Ru core-shell NWs as a function of a length of NWs. (e) A schematic drawing of our proposed mechanism for the propulsion of the Au/Ru core-shell NWs; arrows are represented from the point of view of the nanomotor rather than fluid. The results in (a–d) were obtained from at least 10 independent moving motors in 5 wt % H₂O₂ solution.

travel by convection, diffusion, and migration to the cathode (Ru), where they react with electrons, oxygen, and H₂O₂ molecules to produce H₂O in the reduction process. As a consequence of this redox reaction, protons are asymmetrically distributed around the nanomotor, and an asymmetric electric field is developed. This self-generated electric field causes protons to migrate inside the electrical double layer that naturally forms when the nanomotor is immersed in a water solution. Proton migration leads to an electroosmotic flow, which induces the motion of the nanomotor.

The influence of the electroosmotic mechanism on the locomotion of our core-shell nanomotor was simulated using the commercial multiphysics simulation package COMSOL (5.1).⁴⁸ A number of important results were obtained from the simulation, and served to guide our experiments. First, Figure S2a shows that the proton concentration around the Au/Ru core-shell NW is highly asymmetric, higher near Au end and lower near Ru end, resulting in an asymmetric electric potential distribution as seen in Figure S2b. Consequently, the fluid flows from the anode to the cathode (Figure 2b), hence propulsion of the Au/Ru core-shell NW with its anode end (Au) first. The simulation also reveals that the fluid speed is highest at the interface between the cathode and anode of the core-shell NW, where the majority of the electroosmotic flow occurs (Figure 2b).

One important feature we noticed in our simulation (Figure 2b) was that at the end opposite the anode, the electroosmotic flow can be viewed as a combination of two components: the flow from the anode to cathode and the flow from the surrounding solution to the anode. We further investigated how the length of Au/Ru core-shell NW affects the convergent flow. When the length is sufficiently small (~ 500 nm, Figure 2b (i)), the electric field generated at the anode dominates the overall electroosmotic flow (Figure S2c), and the disturbance to the fluid flow at the tip of the cathode is negligible. At approximately 1.5 μm , a flow reversal at the tip occurs, which is caused by the migration of protons from the surrounding solution to the cathode (Figure 2b (ii)). The reverse flow creates a toroidal vortex near the surface of the NW tip. Further increases in length increase the size of the vortex (Figure 2b (iii), (iv)). The vortex causes an increase in fluidic drag at the tail of the NW, as shown by the negative fluidic speed at the cathode end of the NW (Figure S2d).

Lastly, the nanomotor speeds were calculated from the fluid velocities around the core-shell NWs using the Solomentsev and Anderson model, and their speeds as a function of length of the core-shell NW are plotted in Figure 2c.⁴⁸ Our simulation result shows a clear decrease in motor speed as the core-shell NW length increases, which can be attributed to an increase in drag force with increasing NW length, since a no-slip boundary condition was chosen for the nanomotor surface in the

Table 1. Measured Parameters (D_t , v , D_r , and ω) and Theoretical Values (D_{t0} and D_{r0}) of Au/Ru Core–Shell NWs. The errors are obtained from the fitting

| length (μm) | D_t ($\mu\text{m}^2/\text{s}$) | D_{t0} ($\mu\text{m}^2/\text{s}$) | v ($\mu\text{m}/\text{s}$) | D_r ($\mu\text{m}^2/\text{rad}$) | D_{r0} ($\mu\text{m}^2/\text{rad}$) | ω (rad/s) |
|--------------------------|------------------------------------|---------------------------------------|--------------------------------|--------------------------------------|---|------------------|
| 1.5 | 1.18 ± 0.11 | 0.79 | 11.23 ± 1.30 | 2.36 ± 0.10 | 1.50 | 4.91 ± 0.03 |
| 2.5 | 1.16 ± 0.23 | 0.61 | 19.80 ± 0.31 | 0.65 ± 0.02 | 0.45 | 3.43 ± 0.01 |
| 3.5 | 1.05 ± 0.28 | 0.50 | 30.12 ± 0.25 | 0.17 ± 0.01 | 0.20 | 1.12 ± 0.01 |

simulation. In the following section, we will describe how our experiments confirm and violate these seemingly straightforward simulation results and how such conflict leads to a better understanding of the propulsion mechanism of core–shell NWs.

Catalytic Propulsion of the Au/Ru Core–Shell NWs.

The catalytic locomotion of the Au/Ru core–shell NWs (approximate length of 2.5 μm) in H_2O_2 solution was investigated at various concentrations (0, 0.1, 0.3, 2.5, 5, 10, and 20 wt %). The speeds of the core–shell NWs were found to increase with the concentration of H_2O_2 (Figure 3a), showing the maximum speed of 41 ± 7.6 $\mu\text{m}/\text{s}$ at 20 wt % H_2O_2 . This trend is consistent with both our simulation results and previous findings.^{49–52} A representative core–shell NW trajectory is shown in Figure 3a (i). A large displacement is observed over 4.55 s in the presence of H_2O_2 (5 wt %) in contrast to the control experiment, which was conducted in the absence of H_2O_2 and shows Brownian motion with a very small displacement (Figure 3a (ii)).

To systematically understand the locomotion, we studied the dynamic behavior of the core–shell NW with different lengths (≈ 1.5 , 2.5, and 3.5 μm). For this, at least 10 different motion trajectories with the total duration of about 6 s were recorded for each length. From the trajectories, we calculated mean-square displacement (MSD) up to the time interval of 0.23 s, using

$$\Delta L^2(t) \equiv \langle [\mathbf{r}(t) - \mathbf{r}(0)]^2 \rangle \quad (1a)$$

where $\mathbf{r}(t) = (x(t), y(t))$. Also, mean-square angular displacement (MSAD) was calculated up to the time interval of 1 s, using

$$\Delta \theta^2(t) \equiv \langle [\theta(t) - \theta(0)]^2 \rangle \quad (1b)$$

Then, the MSD and MSAD values were averaged. Translational diffusivity (D_t), translational velocity (v), rotational diffusivity (D_r), and rotational velocity (ω) can be extracted by fitting the MSD and MSAD values in these very short time intervals with quadratic functions as follows. First, D_t and v were extracted from the averaged MSD values with^{29,53}

$$\Delta L^2(t) = 4D_t \Delta t + v^2 \Delta t^2 \quad (2a)$$

Also, D_r and ω were extracted from the averaged MSAD values with⁵³

$$\Delta \theta^2(t) = 2D_r \Delta t + \omega^2 \Delta t^2 \quad (2b)$$

The averaged MSD (or MSAD) data and the fitted lines are plotted as scatter and line type, respectively; MSD in Figure 3b and MSAD in Figure 3c.

For comparison, the translational diffusivity D_{t0} and the rotational diffusivity D_{r0} of passive Brownian motion (*i.e.*, in the absence of H_2O_2) of our core–shell NW are calculated by the Einstein relation:

$$D_{t0} = \frac{k_B T}{f_t^{\parallel}} \quad (3)$$

$$D_{r0} = \frac{k_B T}{f_r^{\perp}} \quad (4)$$

where k_B is the Boltzmann constant, T is the absolute temperature, f_t^{\parallel} is the translational frictional drag force parallel to the long axis, and f_r^{\perp} is the rotational frictional drag force about the short axis of NW with a length (L) and a diameter (d) in a viscous media η . The drag terms f_t^{\parallel} and f_r^{\perp} are defined as⁵⁴

$$f_t^{\parallel} = \frac{2\pi\eta L}{\ln(L/d) - 0.207 + \frac{0.980}{(L/d)} - \frac{0.133}{(L/d)^2}} \quad (5)$$

$$f_r^{\perp} = \frac{\pi\eta L^3}{3\left(\ln(L/d) - 0.662 + \frac{0.917}{(L/d)} - \frac{0.05}{(L/d)^2}\right)} \quad (6)$$

Table 1 shows that the experimental values of D_t and D_r are higher than the theoretical values of D_{t0} and D_{r0} probably due to slight variations in diameters and lengths from sample to sample. Nevertheless, the translational diffusivity D_t , rotational diffusivity D_r , and rotational velocity ω decrease with increasing length. This can be readily explained by the Einstein law: As the length increases, both translational and rotational drag forces increase, which results in a decrease in both the diffusivity and rotational velocity. Importantly, as the length increases from 1.5 to 3.5 μm , the degree of decrease in D_t is notably different from that of D_{t0} , while their D_t decreases in a similar way that of D_{t0} . In other words, core–shell NWs move much more linearly than predicted (see Movie S1). In order to rationalize such a discrepancy in D_r , we turn our attention to the vortex at the tail of the cathode that was found in the numerical model (see again Figure 2b). These vortices were formed by the convergence of flow from different directions. We postulate that such vortex causes additional fluidic drag that stabilizes the NW and contributes to the large reduction in the rotational diffusivity (*i.e.*, higher directionality). To elaborate, for stable propulsion, the center of the drag force should be located behind the center of the thrust, and stability increases with the distance between these two centers. In our case, the center of thrust is located at the tip of the anode (Au), while the center of the drag force, which is normally at the center of volume for the nanomotor, is shifted toward the cathode (Ru) due to the additional drag by vortex at the Ru end. The distance between the two centers increases with the size of the vortex as the length increases, which is consistent with our observation that rotational diffusivity decreases with length.

Contrary to intuition and our simulation results, the speeds (v) of core–shell NWs increased with increasing length (Table 1). The instantaneous speeds, analyzed to confirm the MSD result, also show the same tendency of speed with length (Figure 3d). Such increase in speed with length was found for

micromotors driven by bubble releasing mechanism,⁵⁵ but is completely unexpected for nanorod motors driven by self-electroosmosis. For example, previous studies conducted on Cu/Pt or Au/Pt nanomotors show a decrease in speed with increasing nanomotor length, most likely due to increasing drag force with increasing length.^{21,56} Such an abnormal increase in speed with length, therefore, hints at an additional driving force that increases with length; it superimposes on the main driving force (electroosmotic force), resulting in an increase in the net propulsive force of the nanomotor (Figure 3e). We propose the extra driving force originated from the self-diffusiophoresis mechanism that is popularly used to explain the motion of Janus particles that produce neutral molecules.²⁶ To begin with, besides the electrochemical catalysis of H₂O₂ described at the beginning of our discussion, over 99% of H₂O₂ is believed to undergo chemical decomposition on the Ru surface,⁴⁸ producing a large number of oxygen molecules that establishes an oxygen gradient pointing from Ru to Au. A diffusiophoretic force, then, acts on the oxygen-producing end in the same way as a Pt-SiO₂ Janus particle moving in H₂O₂. We note that a similar geometry of an inert NW with a catalytic manganese oxide tip has been reported to show enhanced diffusion in H₂O₂, indirectly supporting our hypothesis that oxygen gradient can provide an axial force on a cylindrical geometry.⁵⁷

The overall propulsion force for a Au/Ru core-shell NW is therefore a vector sum of the diffusiophoretic and electroosmotic force. Since both forces coincidentally point from Ru to Au in this case, we then expect the diffusiophoretic component to enhance the overall mobility of the core-shell NW. In addition, since this effect increases with the magnitude of the oxygen gradient, a NW with a longer Ru shell would therefore produce more diffusiophoretic force and leads to faster overall propulsion. This explains the seemingly peculiar trend of motor speed increasing with NW length. Although our hypothesis that self-diffusiophoresis due to the generated O₂ concentration on the Ru surface leads to a speed enhancement is intuitive, the exact magnitude of such an enhancement remains unknown. It is, therefore, difficult to directly compare the relative strength from the enhanced propulsive force due to diffusiophoresis to the larger viscous drag for a longer rod.

Catalytic Propulsion of the Core-Shell NWs with Various Material Combinations and the Prediction of Their Propulsive Force. We now attempt to generalize the contribution of diffusiophoresis to other core-shell NWs beyond Au/Ru. Rh and Ru have similar activity toward catalyzing the decomposition of H₂O₂,⁵⁸ but Au/Ru and Au/Rh bimetallic motors move to opposite directions.²² Therefore, by replacing Ru with Rh, we expect to extract more information on how diffusiophoresis influences the motor's behaviors. To this end, we fabricated Au/Rh and Rh/Au core-shell NWs with a total length of 2.5 μm. Their motion in the presence of 20 wt % H₂O₂ was compared with that of Au/Ru core-shell NWs. The trajectories of the core-shell NWs are represented in Figure 4 (right column).

We found that the speeds of these three types of core-shell nanomotors follow the trend of Au/Ru ≫ Rh/Au > Au/Rh (see the Movie S2), which cannot be explained solely by the existing theory of self-electroosmosis. The speed of a self-electroosmotic nanomotor, in general, is determined by a combination of their surface charges (zeta potential) and the self-generated electric field as a result of the surface electrochemical reactions. To understand the effects of these two factors on the speeds of the three types of motors, we first

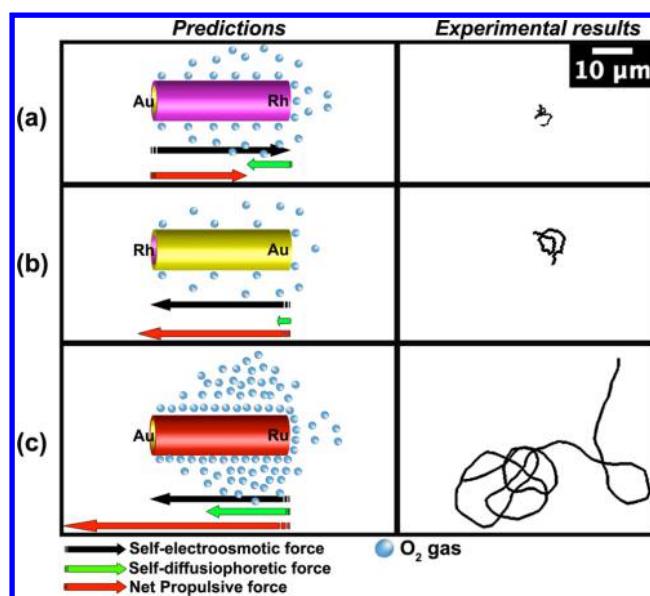


Figure 4. Predictions of the magnitude and direction of self-electroosmotic and self-diffusiophoretic forces and the experimentally observed tracked paths of (a) Au/Rh, (b) Rh/Au and (c) Au/Ru core-shell NWs over 4.8 s. The arrow magnitudes are relatively predicted in three samples, and force arrows are represented from the point of view of the nanomotor rather than fluid.

measured the zeta potential of Au/Ru, Rh/Au, and Au/Rh core-shell NWs, all yielding results of approximately -26 mV. The difference of surface charges is therefore eliminated as a possible reason to explain their speed variations. Second, given a previous study by Wang *et al.*²² showing similar speeds of Au/Ru, Rh/Au, and Au/Rh segmented NW motors, we believe the difference in the self-generated electric field by these three samples is insignificant. In addition, one may wonder if the speed differences among these three types of motors could have originated from varying degrees of core protrusion where a small segment of the core metal is exposed, as shown in Figure S4a. However, our simulation results show that the effect of the protrusion is too small to account for the large speed variation. A detailed discussion can be found in the Supporting Information. To briefly summarize, the self-electroosmotic mechanism predicts similar speeds for these three samples, which is in clear contrast to what we have experimentally observed.

Given the inadequacy of self-electroosmosis in explaining the observed speed trend, we attempt to reconcile our results with self-diffusiophoresis that successfully explained the behaviors of Au/Ru core-shell nanomotors. The magnitude of the self-diffusiophoretic force, *i.e.*, the additional driving force, depends on the O₂ concentration gradient developed by the decomposition of H₂O₂ on the catalytically active layer. According to previous studies, the decomposition rate of H₂O₂ on Ru is twice as high as Rh, while it is 10 times lower on Au than on Rh.⁵⁸ Thus, the predicted magnitude of the self-diffusiophoretic forces on core-shell NWs of equal lengths follows Au/Ru ≫ Au/Rh > Rh/Au (shells being Ru, Rh and Au, respectively), provided that the total amount of H₂O₂ decomposition is defined as the product of the decomposition rate and the reactive surface (shell) area. The diffusiophoretic force directions on Au/Rh, Rh/Au, and Au/Ru core-shell nanomotors can be predicted as Rh → Au, Au → Rh, and Ru → Au, respectively. The predicted force magnitudes and

directions of the above three motors are illustrated in the left column of Figure 4 and compared to experimental results (right column). The relative speeds of these three nanomotors are estimated by comparing the magnitudes of the propulsive forces that is the sum of the electroosmotic and diffusiophoretic forces. Our prediction is in reasonable and qualitative agreement with our experimental observation, lending support to the combined propulsion mechanism we proposed.

CONCLUSIONS

In conclusion, Au/Ru core-shell NWs have been fabricated by electrodeposition and studied as a catalytic nanomotor when submerged in H₂O₂. Their maximum speed was observed to be $41 \pm 7.6 \mu\text{m/s}$ in 20 wt % H₂O₂. Decreased rotational diffusivity or, equivalently, enhanced directionality is observed with increased length, which likely results from the formation of vortices at the Ru end of the NW, as revealed by numerical simulation. Interestingly, this nanomotor design exhibits a positive length-speed correlation, which is contrary to the previously reported rod-shaped nanomotor systems or our own simulation results. We reconcile such a conflict by hypothesizing that the overall propulsion originates from two simultaneous mechanisms, namely self-diffusiophoresis and self-electroosmosis. For a core-shell Au/Ru NW, the self-diffusiophoretic force, originated from the oxygen produced at Ru surface, is superimposed on the self-electroosmotic force in the same direction, increasing the net motor speed. In addition, when the catalytic active surface area (Ru) increases with length, the self-diffusiophoretic force increases due to a higher O₂ concentration gradient, leading to a higher motor speed. The proposed propulsion mechanism also justifies the large difference in speed among Au/Rh, Rh/Au, and Au/Ru core-shell NWs, which is not observed for conventional bimetallic NWs of similar compositions. Through careful experimental designs and the adopted fabrication strategy, we reveal the possible role of self-diffusiophoresis on propelling a widely studied nanomotor system. Although the exact magnitude of this force remains yet to be uncovered, we have reason to believe that this finding will advance our understanding of forces on nanomotors and help reconcile noncooperating experimental results. Self-diffusiophoresis, although popular in other nanomotors systems, has been traditionally ignored in bimetallic nanomotors. We are once again reminded of the complex interplay between diffusiophoresis and electroosmosis and call for a renewed attention on this matter.⁵⁹

METHODS/EXPERIMENTAL

AAO-Si Wafer Bonding: A Platform for the Fabrication of Core-Shell NWs. An AAO (Anodisc 25, 200 nm, Whatman, 200 nm) membrane and Si chip (2 cm × 2 cm) were sonicated in acetone, isopropanol, and distilled (DI) water for 10 min to remove organic residuals. An additional cleaning process was conducted for the Si chip. This consists of dipping and sonicating the Si chip in piranha solution (7:3 H₂SO₄:H₂O₂) for 10 min. Note that the piranha solution is a strong oxidizer, which requires great care in handling. The cleaned AAO and Si chip were further coated with a Au layer of a thickness of 500 nm by means of thermal evaporation (EDWARD, U.K.) at 1×10^{-6} mTorr. The coated AAO was, then, transferred to the coated Si substrate *via* Au/Au compressive bonding at 1×10^{-5} mTorr, 1 M Pascal, and 320 °C for 15 min.

Fabrication of Au/Ru Core-Shell. The bonded AAO membrane was then subjected to electrodeposition to grow Au/Ru core-shell NWs as follows. Au NWs were electrochemically deposited in the

nanopores of AAO at -2 mA cm^{-2} for 90 min. The Au bath consisted of gold(I) potassium cyanide (AuK(CN)₂, 8 g L⁻¹), citric acid (C₆H₈O₇, 90 g L⁻¹), potassium citrate (C₆H₅K₃O₇, 90 g L⁻¹), and 10 mL L⁻¹ of a brightener concentrate which contained cobalt(II) carbonate as a grain refiner (0.05 g L⁻¹). After the core deposition, the AAO membrane was selectively etched in 5 M NaOH for 2 h, resulting in the formation of freestanding Au NW arrays on the Si substrate. After etching the AAO, the standing array was thoroughly rinsed with DI water to remove residuals for Ru shell deposition. The shell was galvanostatically deposited at -0.5 mA cm^{-2} for 10 min in a Ru bath (pH 1.2). The bath consisted of 0.05 M of RuCl₃, and the pH of the bath was adjusted by adding HCl (37 wt %). After the Ru deposition, the Au/Ru core-shell NWs were released by sonication in DI water.

Characterization. SEM images were acquired by a backscattering electron detector in Zeiss ULTRA 55. HAADF STEM images and EDX maps were acquired using FEI Talos F200X under an accelerating voltage of 200 kV.

Manipulation. We investigated catalytic locomotion of our core-shell NWs in H₂O₂ under an inverted optical microscope equipped with an objective lens of 40×. Image sequences were recorded using a CCD camera at 30 fps.

Numerical modeling. The numerical modeling was performed using the commercial multiphysics simulation package COMSOL (5.1). In the simulation, 2D axisymmetric model was selected, and geometry of a nanomotor was defined as a simple rod that has a diameter of 300 nm and a length of 2.5 μm. To study the length effect, the length of rod varied as 0.5, 1.5, 2.5, and 3.5 μm. Diluted species transport, electrostatic, and creeping flow models were coupled to compute proton concentration, electric potential, and fluid flow around the core-shell NW. The size of mesh was selected to be $1 \times 10^{-6} \mu\text{m}$ and $5 \times 10^{-7} \mu\text{m}$ for maximum and minimum element size, respectively. The detailed physics and boundary conditions are noted in Supporting Information S2.

ASSOCIATED CONTENT

Supporting Information

The Supporting Information is available free of charge on the ACS Publications website at DOI: 10.1021/acsnano.6b04224.

Movie S1: A motion comparison of Au/Ru core-shell nanowires at different lengths (AVI)

Movie S2: A motion comparison among Au/Rh, Rh/Au and Au/Ru core-shell nanowires (AVI)

Numerical modeling procedures and additional numerical modeling results of the effect of core protrusion on the speed of nanomotors and supporting figures (PDF)

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Author Contributions

S.P. and B.J.N. initiated the project. S.P. and B.J. designed the fabrication experiments. B.J. and S.W. fabricated the magnetic nanoswimmers and analyzed their motion. W.W., B.J., and C.H. conducted the simulation experiments. B.J., W.W., A.P., X.C., A.H., B.J.N., D.F., and A.F. performed the analysis of the swimmers and provided theoretical discussion. B.J., W.W., A.P., X.C., S.P., and B.J.N. supervised the work and gave critical input.

Notes

The authors declare no competing financial interest.

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